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# Aerosol filtration efficiency of household materials for homemade face masks: Influence of material properties, particle size, particle electrical charge, face velocity, and leaks

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As a consequence of the COVID-19 pandemic caused by the SARS-CoV-2 virus the widespread daily use of face masks is promoted worldwide. Particle-size dependent filtration efficiencies ( $FE$ ;  $d_p=30\text{ nm} - 10\text{ }\mu\text{m}$ ), applying a particle counting approach, and additionally pressure drops ( $\Delta p$ ) were determined for 44 samples of household materials and several medical masks. Huge  $FE$  differences were found between sample materials and for different particle sizes, spanning from  $<10\%$  up to almost  $100\%$ . Minimum  $FE$  were determined for  $d_p=50 - 500\text{ nm}$  particles with significantly larger values for  $d_p=30\text{ nm}$  particles and especially for those with  $d_p>2.5\text{ }\mu\text{m}$ . Measurements at different numbers of layers showed that stacks of textiles can be treated as separate filters and total  $FE$  and  $\Delta p$  can readily be estimated from the features of the individual layers, leaving laborious measurements of individual combinations obsolete. For many materials, electrostatic attraction contributes strongly to overall  $FE$  for particles up to  $100\text{ nm}$  diameter. Measurements with defined leaks showed that already a small fractional leak area of  $1\text{-}2\%$  can strongly deteriorate total  $FE$ . This is especially the case for particles smaller than  $5\text{ }\mu\text{m}$  diameter, where  $FE$  dropped by  $50\%$  or even two thirds. Our measurements show that by stacking an adequate number of layers of many fabrics, decent filtration efficiencies can be reached for homemade face masks over large particle size ranges with acceptable pressure drop across the material. Very important, however, is good fit of the masks to minimize leak flows and selection of non-hazardous mask material.

## 1 Introduction

Within months, the current corona virus disease 2019 (COVID-19) pandemic has spread over the whole planet. As a consequence of this massive outbreak, social and economic life is severely affected in many countries (Leopoldina 2020) due to a combination of widespread lockdowns as well as physical and social distancing measures, recommended or enforced by national health authorities and politics (Zhang et al. 2020).

COVID-19 spreads via transmission of the severe acute respiratory syndrome coronavirus 2 (SARS-CoV-2), involving virus-containing respiratory fluids and saliva (WHO 2020a). The World Health Organization (WHO) has suggested that the primary transmission modes of SARS-CoV-2 are person-to-person transmission (i.e., droplet transmission) and contact with contaminated surfaces (WHO 2020a, 2020c). The rapid spread of the virus as well as various studies, e.g., showing transmission over distances  $>1\text{-}2\text{ m}$  (Li et al. 2020), however, suggest that also other routes of transmission such as airborne transmission may play an important role (Hadei et al. 2020; van Doremalen et al. 2020; Morawska and Milton 2020; Zhang et al. 2020). The corresponding details, however, are not completely known yet (Morawska and Milton 2020; Zhang et al. 2020; Hadei et al. 2020; Klompas et al. 2020).

Droplet transmission is based on respiratory droplets, which, according to WHO convention (Gratton et al. 2011; WHO 2014; Kutter et al. 2018), have a diameter ( $d_p$ ) of  $5\text{ }\mu\text{m}$  and larger. Contact (or fomite) transmission can occur via deposition of virus-containing respiratory fluids on surfaces when

they are touched by a person who subsequently touches the own nose, mouth or eyes (WHO 2014). In airborne (or aerosol) transmission, the virus is transported via droplet nuclei or smaller aerosol particles ( $d_p \leq 5 \mu\text{m}$ ) suspended in air (WHO 2014), which can stay suspended in air over extended periods of time (Hinds 1999). Airborne transmission requires that the virus remains infectious in droplet nuclei over extended time periods. This is known to be the case for pathogens causing pulmonary tuberculosis, measles, or chickenpox (WHO 2014), however also for SARS-CoV-2 viability in aerosol particles over more than an hour has been demonstrated (van Doremalen et al. 2020).

Exhaled respiratory particles cover a particle size range from  $d_p = 0.01 \mu\text{m}$  up to  $1000 \mu\text{m}$  (Gralton et al. 2011; Bake et al. 2019 and references therein), generated by coughing and sneezing, but also during speaking and regular breathing (Chao et al. 2009; Morawska et al. 2009; Johnson et al. 2011; Bake et al. 2019). Breathing generates the smallest particles (typically  $d_p < 4 \mu\text{m}$ ) with a mode diameter around  $0.8 \mu\text{m}$ , caused by fluid film burst during airway reopening (Bake et al. 2019; Johnson et al. 2011), with particle concentrations increasing with exhalation depth (Bake et al. 2019). Slightly larger particles were observed from whispering and speaking with more particles being generated from voiced activities than from whispered (Morawska et al. 2009). These particles as well as those from coughing are generated by vocal cord vibrations and aerosolization in the laryngeal region; their count mode diameters were found to be around  $d_p = 1 \mu\text{m}$  (Johnson et al. 2011) or  $6 \mu\text{m}$  (Chao et al. 2009). Their concentrations were found to be an order of magnitude higher than those from breathing (Morawska et al. 2009), increasing with speech loudness (Asadi et al. 2019). Much larger droplets are generated in the upper respiratory tract during speaking, coughing and sneezing with  $d_p$  around  $200 \mu\text{m}$  (Johnson et al. 2011).

The fate and hazardousness of potentially virus-containing droplets after exhalation strongly depends on their size. Small droplets, smaller than several tens of  $\mu\text{m}$ , evaporate within seconds (Morawska et al. 2009; Gralton et al. 2011; Parienta et al. 2011; Chaudhuri et al. 2020), leaving droplet nuclei of 30-50% of their initial diameter, depending on the amount of dissolved material. Droplet nuclei with  $d_p < 10 \mu\text{m}$  can remain airborne over extended periods of time and can be inhaled, with smaller particles reaching deeper regions of the respiratory system (Oberdörster et al. 2005). Very large droplets,  $d_p > 100 \mu\text{m}$ , sediment quickly and are mostly deposited on a surface before they evaporate (Chaudhuri et al. 2020). The number of virions within a single respiratory particle depends on the virus titer in the source region and increases with the cube of the particle diameter. With SARS-CoV-2 viral loads of  $4.6 \cdot 10^5$  copies per mL of nasopharyngeal sample (Bae et al. 2020), about 20% of exhaled  $100 \mu\text{m}$  diameter droplets would contain a virion; for  $10 \mu\text{m}$  droplets only 2 out of 10,000 particles would contain a virion and for  $d_p = 1 \mu\text{m}$  droplets this fraction would be another 1000 times smaller.

To prevent transmission of COVID-19, the wearing of face masks in addition to thorough hand hygiene and physical distancing is advised (e.g., WHO 2020b; Leopoldina 2020). Health workers are recommended to wear a surgical mask, certified according to a set of test methods like European standard EN 14683, or filtering facepiece respirators (FFR), certified for filtration efficiency and seal leakage rate according to test procedures like European standard EN 149 (e.g., FFP2), which protect the wearer (Lee et al. 2008; Oberg and Broussau 2008). Under conditions of severe medical mask supply shortage, the use of cloth masks is recommended for the general public only (WHO 2020b).

The massive demand for medical masks during the first months of the pandemic caused shortage of supply of such devices in many countries. Therefore, numerous people make their own cloth masks using various kinds of available fabrics. In addition, new suppliers of simple cloth masks mushroom, frequently offering masks of questionable filtration efficiency and quality. Furthermore, in many countries suffering from poor air quality, people wear simple cloth masks to protect themselves from particulate air pollution (Shakya et al. 2017; Neupane et al. 2019), known to cause various adverse health effects (Jacobson 2012; WHO 2016).

Particle removal from an airstream is caused by five physical mechanisms: interception, inertial impaction, gravitational settling, diffusion, and electrostatic attraction (Hinds 1999). While the first three mechanisms increase in efficiency with increasing particle size, the latter two are more efficient for smaller particles. This results in typical filtration efficiency curves with a minimum for particles of around 0.05  $\mu\text{m}$  to 0.5  $\mu\text{m}$  diameter (most penetrating particle size, Hinds 1999). Larger face velocities cause an increase of deposition by impaction, however gravitational settling, diffusion, and electrostatic attraction become less efficient under such conditions.

Both applications of cloth masks, protection from respiratory disease transmission and from particulate air pollution, require the removal of particles within a large size range. Exhaled respiratory particles range in diameter from 0.01  $\mu\text{m}$  to 1000  $\mu\text{m}$  (Bake et al. 2019) with particles smaller than  $\sim 10 \mu\text{m}$  in diameter being respirable. Urban air pollution contains ultrafine particles ( $d_p < 100 \text{ nm}$ ), e.g., diesel soot particles, fine particles ( $d_p < 1 \mu\text{m}$ ) with secondary pollutants, as well as coarse particles ( $d_p > 1 \mu\text{m}$ ), often consisting of mineral dust and sea salt (e.g., Jacobson 2012 and references therein).

Several studies on filtration efficiency of simple cloth masks or fabrics which can be used to make such masks can be found in the literature (Rengasamy et al. 2010; Davies et al. 2013; Shakya et al. 2017; Neupane et al. 2019; Konda et al. 2020; Lustig et al. 2020). These studies present results only for a very limited variety of materials with no or only little systematic investigation of factors influencing particle filtration efficiency. Therefore, in order to support the selection of adequate materials for making cloth face masks and to better understand which factors affect mask efficacy, we performed systematic measurements of particle size-resolved ( $d_p = 30 \text{ nm} - 10 \mu\text{m}$ ) filtration efficiency and of pressure drop for 44 typical household materials and several medical masks under different experimental conditions, including different face velocities, number of sample layers, and leaks.

## 2 Methods and materials

Filtration efficiency of sample materials was determined by measuring particle transmission through the respective samples, applying different particle counting methods: the *CPC setup* (Condensation Particle Counter setup) for measurement of electrically charged and neutralized aerosol particles in the diameter range from 30 nm up to 500 nm; and the *SMPS/OPC setup* (Scanning Mobility Particle Sizer/Optical Particle Counter setup) using ambient aerosol particles ( $d_p = 30 \text{ nm} - 10 \mu\text{m}$ ).

### 2.1 Design of the CPC setup

The *CPC setup* is presented schematically in Fig. 1a. NaCl aerosol is generated using a nebulizer (model 3076, TSI, Inc.) and a silica gel diffusion dryer. A differential mobility analyzer (DMA, model 3081, with X-ray aerosol neutralizer model 3088, both TSI, Inc.) is used to generate monodisperse aerosol of the desired  $d_p$ . Note that this provides mobility particle diameter (i.e.,  $d_p = d_{mob}$ ), which is used throughout this manuscript. The resulting aerosol is either directly used (“charged aerosol”) or it is directed through an additional aerosol neutralizer (model 5522-A, Grimm Aerosoltechnik) to bring the aerosol into the natural charge equilibrium again (“neutralized aerosol”). After dilution with particle-free air and turbulent mixing of sample and dilution flow in a 15 cm long piece of  $\frac{1}{4}$ ” tubing the aerosol passes the sample (i.e., the mask or cloth material), fixed in a sample holder (ID=65 mm). The flow through the sample is maintained using a vacuum pump (model V-VTE-10, Rietschle) and an adjustable valve and measured using a thermal mass flow meter (model 4043, TSI, Inc.). In front of and behind the sample holder, partial flows of the aerosol are diverted to two water-based CPCs (model 3787, TSI, Inc.) in order to measure respective particle number concentrations. The pressure difference across the sample is measured using a differential pressure sensor (model testo 440 dP, Testo SE & Co. KGaA).

Figure 1

## 2.2 Design of the SMPS/OPC setup

For measurement of filtration efficiencies for particles up to  $d_p=10\text{ }\mu\text{m}$ , the *SMPS/OPC setup* (Fig. 1b) was adopted, using ambient aerosol, which entered the room through an open gate. The aerosol was drawn through the sample, which was fixed onto a flange (ID=70 mm) on the top of a 20-liter flow chamber. The flow was maintained using a vacuum pump (model SH-110, Varian, Inc.) connected to the bottom of the flow chamber in combination with an adjustable valve and a thermal mass flow meter (model 4043, TSI, Inc.). Particle size distributions in the diameter range from 250 nm up to more than 10  $\mu\text{m}$  were measured simultaneously with two OPCs (model 1.109, Grimm Aerosoltechnik). The two instruments used vertical inlet lines ( $l=50\text{ cm}$ ) with inlet openings in the center of the flow chamber and next to the flow chamber inlet in ambient air, respectively. In addition, particle size distributions ( $d_p=20\text{ nm} - 450\text{ nm}$ ) were measured using a single SMPS system, alternating between two inlet lines with openings in and next to the flow chamber. The SMPS consisted of an X-ray aerosol neutralizer (model 3088, TSI, Inc.), an electrostatic classifier (model 3082, TSI, Inc.) with a differential mobility analyzer (model 3081A, TSI, Inc.), and a nano water-based CPC (model 3788, TSI, Inc.).

## 2.3 Sample materials

A total of 48 different sample materials were investigated:

- twelve pure cotton fabrics, including woven textiles with different thread counts as well as jersey and velvet cotton,
- five fabrics containing cotton mixed with synthetics, including flannel, French terry, and velour,
- eleven synthetic fiber samples including woven and jersey materials,
- four paper-like materials (paper towels, coffee filter, paper tissue),
- four natural fiber materials (linen, wool, silk),
- eight synthetic household materials such as vacuum cleaner bags, a vacuum cleaner bag backup filter, anti-allergic mattress and linen encasements, and polyurethane (PU) foams,
- three commercially available surgical masks (EN 14683) and one FFP2 mask (EN 149); a separate surgical mask (EN 14683) was used for the measurements of the influence of leaks on filtration efficiency.

A list of all sample materials with details like thread count, material area density, and composition is provided in the supplementary information (SI, Table S1). As customary in the textile industry, for woven materials, thread count was determined as the sum of warp and filling threads in one square inch of the textile. For knitted materials we determined an estimate of the thread count by counting the number of stitches along the base and the height of the same square and multiplication by three to account for the number of threads confining each stitch. Material area density (in  $\text{g m}^{-2}$ ) was determined by weighing a 20 mm diameter punch of the material and expanding this value to the mass per square meter. For the analysis, both numbers were multiplied with the numbers of layers of the material used for the measurements. When mounting stretchable fabrics in the sample holder, special care was taken not to expand them.

## 3 Test procedure and analysis

### 3.1 Measurements and data analysis for the CPC setup

One CPC measured upstream and one downstream the sample for 30 s (1-s time resolution), then the CPCs were swapped for another 30 s measurement to account for potential instrumental differences. The transmission  $T$  was calculated as the geometric mean of the ratio of measured downstream to upstream concentrations of both measurements, and corrected for setup-inherent particle losses by multiplying with an experimentally determined correction factor of 0.99. Each measurement was divided into three subsets and repeated three times with freshly mounted sample material, resulting in a total of nine measurements of which the average and as measurement uncertainty the 1-sigma standard deviation of the average were calculated. All measurements were performed with particles of 30 nm, 50 nm, 100 nm, 250 nm, and 500 nm diameter, for both charged and neutralized aerosol, at two flow rates which correspond to face velocities at the filter of  $5.3 \text{ cm s}^{-1}$  and  $12.9 \text{ cm s}^{-1}$ , respectively. For more details, see SI (Sect. S1).

Pressure drop  $\Delta p$  across the sample was measured threefold after stabilization of the reading and corrected for the flow resistance of the tubes between the pressure gauge connections, determined at the same flow with no sample installed. Uncertainty of  $\Delta p$  was typically 1 Pa.

### 3.2 Measurement and data analysis for the SMPS/OPC setup

After 5 min equilibration time, SMPS and OPC measurements were performed in parallel: while the two OPCs sampled for ~20 min at 6-s time resolution filtered and ambient air, respectively, providing three subsets of ~7 min each, the SMPS was switched between the two air flows after each 150 s scan, resulting in three ambient/filtered air sample pairs per measurement. This measurement was repeated three times with a newly mounted sample, providing nine individual values of filtration efficiency in total. Size-resolved filtration efficiencies  $FE$  (defined as  $FE[\%] = 100 \cdot (1 - T)$ , with transmission  $T$  the ratio of average particle number concentration at a given diameter measured in filtered to that in ambient air) were calculated individually from the SMPS and OPC measurements. Afterwards they were merged to a single filtration efficiency curve. From this curve,  $FE$  for the chosen particle diameters (30 nm, 50 nm, 100 nm, 250 nm, 500 nm, 1  $\mu\text{m}$ , 2.5  $\mu\text{m}$ , 5  $\mu\text{m}$ , and 10  $\mu\text{m}$ ) were obtained. Instrumental differences between the OPCs were accounted for by applying an experimentally determined size-dependent correction factor. All measurements were performed at the two face velocities also used in the *CPC setup*. More details are provided in the SI (Sect. S2).

In addition to the standard deviation of the average, also the uncertainty due to counting statistics (dominating uncertainty at low particle number concentrations) was calculated for each particle size. Provided in the results section are always the larger of the two uncertainty values.

## 4 Results

### 4.1 Overview of filtration efficiencies of masks and potential mask materials

Exemplary filtration efficiency curves for both face velocities are shown in Fig. 2 for jersey (2 layers), velvet polyester, vacuum cleaner bag (#2), and silk (thin). Filtration efficiency curves for all materials are shown in the SI (Figs. S1 to S7). As expected from filtration theory (see Sect. 1; Hinds 1999), a minimum in  $FE$  is found between 50 nm and 500 nm for all samples. More efficient diffusion and electrostatic attraction for smaller particles, and interception, impaction and gravitational settling for larger particles result in larger  $FE$  towards both ends of the probed size range. The absolute level of filtration efficiencies for particles of individual diameters as well as the diameter of minimum efficiency depend on the respective efficiency of the various deposition mechanisms. For increased face velocity, diffusion and electrostatic attraction (mainly affecting very small particles) are less effective while impaction (mainly affecting large particles) is more effective. This causes a shift of the diameter of minimum  $FE$  towards smaller particles, reduced  $FE$  values for

very small particles, and increased *FE* for the larger particles for higher face velocity (Fig. 2 and Figs. S1 to S7).

Figure 2

A very large spread in filtration efficiencies was observed for all particle sizes between the various materials and even between the different surgical masks (Fig. S7). For many samples, high filtration efficiency for large particles was found: more than 30 of the samples have *FE* >80% for particles with  $d_p \geq 5 \mu\text{m}$ . In contrast, only few samples showed good filtration efficiency for very small particles: only six samples at the lower and even fewer at the higher face velocity filtered >80% of 30 nm diameter particles. In the filtration minimum only seven samples were able to filter >50% of the particles at the higher face velocity; all these materials were nonwoven materials like medical masks, mattress encasement, vacuum cleaner bags, and backup filter.

Figure 3

For direct comparison of all sample materials, *FE* bar charts for each particle size are presented in the SI (Figs. S9 to S22). Since particle deposition for particles with sizes below or above the filtration minimum is dominated by different mechanisms, we calculated average filtration efficiencies for both particle size ranges (*small particles*:  $d_p=30 \text{ nm} - 250 \text{ nm}$ ; *large particles*:  $d_p=500 \text{ nm} - 10 \mu\text{m}$ ) for simpler comparison of potential mask materials (Figs. 3 and S8 for low and high face velocity, respectively). The pressure drop across the sample material was determined for standard flow conditions (i.e.,  $8 \text{ L min}^{-1}$  flow rate through a sample of  $25 \text{ mm}$  diameter) as defined for certification of surgical face masks in the European standard EN14683 (2019). According to this standard, these pressure drops are calculated by dividing the measured pressure drop by the sample area ( $4.9 \text{ cm}^2$ ) and are provided in units of  $\text{Pa cm}^{-2}$  (Fig. 3c).

*FE* for small particles (Fig. 3a and Fig. S8) are presented for completely charged, neutralized, and ambient aerosol. For materials with charged fibers, electrostatic attraction can enhance *FE* for particles in this size range. Therefore, enhanced *FE* for the charged aerosol is a good indication that the respective sample material contains either permanently or temporarily (e.g., due to the handling of the material) electrostatic charges on its fibers. Almost all materials which show such behavior consist completely or largely of synthetic components. The only exceptions to this are velvet cotton and thin silk, which are made of pure cotton and silk, respectively, and show slightly higher filtration efficiency for charged aerosol, compared to incompletely charged aerosol.

The largest *FE* were mostly found for samples with a strong electrostatic deposition component. However, a strong electrostatic deposition component is not a guarantee for good filtration efficiency. Several samples like flannel, thin silk, swimsuit, or the triangle bandage show enhanced filtration efficiency for charged particles, albeit at rather low overall *FE* level (Fig. 3a). Generally, filtration efficiency for ambient, i.e., incompletely charged, aerosol is relatively low for small particles with only four samples (vacuum cleaner bag #2, encasement #1, FFP2, and surgical mask #2) exceeding 80% *FE* on average. Extremely low filtration efficiencies (polyester, polyester with elastane, woven cotton, cotton shirt, silk, linen, polyurethane foam samples) are associated with either thin or rather open material structures, i.e. with materials with high porosity.

Filtration efficiencies for large particles (Fig. 3b) are typically larger than those for small particles (Fig. 3a). Especially for the largest particles used in this study ( $d_p=5 \mu\text{m}$  and  $10 \mu\text{m}$ ) *FE* approaching 100% were found for many samples (Figs. S21 and S22). Unsurprisingly, the largest filtration efficiencies were mostly found for materials which were specifically designed for the purpose of filtering particles, like vacuum cleaner bags or medical masks. However, also many other materials show substantial filtration capability (*FE*  $\geq 50\%$ ) for the large particle size range. Therefore, these could be useful in masks if it is intended to remove larger respiratory droplets from the air flow.

The best filtration efficiency is not very helpful for making a cloth mask if it is too hard to breathe through the respective material. Even though all samples were selected as potential candidates for making cloth masks, e.g., from the point of view of material strength or sample material thickness, very significant differences were found in the measured pressure drop values (Fig. 3c). Three self-made masks made of mattress encasement and of poplin combinations showed the largest pressure drop values of ca. 150 to 200 Pa cm<sup>-2</sup>. Many of the other samples ranged between 20 and 50 Pa cm<sup>-2</sup>, where also the surgical masks can be found. A few samples like muslin, a microfiber cloth, vacuum cleaner bag backup filter, triangle bandage, polyester with elastane, and PU foam were very easy to breathe through with pressure drop values below 10 Pa cm<sup>-2</sup>.

#### 4.2 Dependence of filtration efficiency and pressure drop on face velocity and number of layers

To determine the relationships between face velocity, number of layers of the material, pressure drop, and filtration efficiency, we performed a number of systematic measurements. For a selection of four materials (cotton jersey, cotton woven, molleton, and polyester) we measured  $FE$  and  $\Delta p$  for samples with different number of layers (one to five) with low and high face velocity and, for one and two layers, with different face velocities (2.8, 5.3, 9.1, 12.9, 25.4 cm s<sup>-1</sup>). These materials were selected because they showed sufficiently low  $FE$  and  $\Delta p$  for a single layer that also allows reasonable measurements at samples of five layers. In addition, they covered both, woven and non-woven materials, and several of them are of general relevance for self-made face masks.

Figure 4

As expected, with increasing face velocity, we observed an increase in pressure drop across the sample (Fig. 4a). This reflects that it is harder to breathe through the material of the face mask when the respiratory flow is larger. Since the measured pressure drop values for single layered samples were consistently half the values of the double layered samples, we only present results for the latter ones, which have smaller relative uncertainty due to higher  $\Delta p$  levels. A power law function

$$\Delta p(v_f) = \Delta p(0) + A_{\Delta p} \cdot v_f^s \quad (1)$$

was fitted, with  $\Delta p(v_f)$  the pressure drop in Pascal at face velocity  $v_f$  (in cm s<sup>-1</sup>),  $A_{\Delta p}$  (in Pa) the magnitude of the pressure drop increase with increasing  $v_f$ , and  $s$  the exponent describing the shape of the increase (see Table S2 for the individual fitting coefficients). For cotton jersey, the pressure drop curve flattens ( $s=0.80$ ) probably due to widening of the stitch openings at higher flow rates. For the other materials,  $s$  is above unity.

For small particles ( $d_p \leq 250$  nm),  $FE$  decreases with increasing face velocity (Fig. 4b for  $d_p=30$  nm), reflecting reduced particle deposition by diffusion and electrostatic attraction, due to reduced residence times within the filter material. Conversely, for large particles ( $d_p \geq 2.5$  μm)  $FE$  increases with increasing face velocity (Fig. 4d for  $d_p=2.5$  μm), due to enhanced impaction deposition at larger particle velocities. For both particle size ranges,  $FE$  dependence on face velocity  $v_f$  follows an exponential function reasonably well:

$$FE(v_f) = FE_{asympt} + A_{FE} \cdot \exp\left(-\frac{v_f}{\tau}\right) \quad (2)$$

with  $FE_{asympt}$  the asymptotic filtration efficiency (in %) for very large  $v_f$  (given in cm s<sup>-1</sup>),  $A_{FE}$  (in %) the magnitude and  $\tau$  (in cm s<sup>-1</sup>) the  $v_f$  sensitivity of the filtration efficiency dependence. For the smaller particles ( $d_p \leq 250$  nm, Table S3),  $A_{FE}$  is positive and  $FE$  decreases with increasing  $v_f$ , approaching the asymptotic filtration efficiency. Generally, in this particle size range,  $FE_{asympt}$



decreases with increasing particle size (range: 20% – 50% for  $d_p=30$  nm opposed to 7% – 22% for  $d_p=250$  nm). For the larger particles ( $d_p \geq 2.5$   $\mu\text{m}$ , Table S4),  $A_{FE}$  is negative and  $FE$  increases with increasing face velocity. For almost all samples,  $FE_{asympt}$  approaches 100%, especially for the larger particles (i.e.,  $d_p=5$   $\mu\text{m}$  and 10  $\mu\text{m}$ ). This suggests improved filtration efficiencies for such particles under conditions where large face velocities occur, such as during coughing, sneezing or heavy breathing, for the fraction of the air flow that passes through the mask material.

For an intermediate particle size range (Fig. 4c for  $d_p=500$  nm), a transition occurs from decreasing  $FE$  with increasing face velocity in the lower  $v_f$  range to an increase in  $FE$  with face velocity in the upper  $v_f$  range. With increasing particle diameter, we observe a decrease in the face velocity where this transition occurs, in agreement with classical filtration theory (Hinds 1999).

Figure 5

Pressure drop dependences on the number of layers of sample material show a tight linear relationship (Fig. 5a for  $v_f=5.3$   $\text{cm s}^{-1}$ ; see Table S5 for fitting coefficients). For zero layers one would expect  $\Delta p=0$  Pa. This was observed for cotton woven and molleton. For polyester and cotton jersey, however, a significant, albeit small, residual  $\Delta p$  was calculated equivalent of  $\frac{1}{4}$  to  $\frac{1}{7}$  layer of the material. Generally, however, in good approximation the observed pressure drop across the complete sample is proportional to the number of layers of the material.

Filtration efficiency increases with the number of sample material layers. To test whether this dependence is in agreement with classical filtration theory (Hinds 1999), we used particle transmission ( $T=1 - FE[\%]/100$ ). Particle transmission  $T$  dependence on number of layers  $n$  for all four material samples (see Fig. 5b for  $d_p=1$   $\mu\text{m}$  and  $v_f=5.3$   $\text{cm s}^{-1}$ ) can reasonably well be fitted according to the following simple relationship:

$$T(n) = T(1)^n \quad (3)$$

with  $T(1)$  the transmission for a single layer of material. A comparison of measured and fitted values for the single-layered material is provided in Table S6 for all four materials, all measured particle sizes as well as the lower and the higher face velocity.

We conclude that in good approximation the individual layers can be treated as separate filters which are connected in series and which do not interfere with each other strongly, e.g., due to alignment of layers. Therefore, the total pressure drop across the whole sample can be calculated by adding the pressure drops of the individual layers (Eq. 4), and the total transmission efficiency can be calculated by multiplying the transmission efficiencies of the individual layers (Eq. 5). This enables to calculate total pressure drop  $\Delta p_{total}$  and total filtration efficiency  $FE_{total}$  for cloth masks made of an arbitrary combination of layers  $L_i$  of textiles from the features of the individual components:

$$\Delta p_{total} = \Delta p_{L1} + \Delta p_{L2} + \dots \quad (4)$$

$$FE_{total} = 1 - (T_{L1} \cdot T_{L2} \cdot \dots) \quad (5)$$

This approach supersedes performing laborious measurements of filtration efficiency for combinations of materials in order to determine their suitability as basis for self-made face masks.

### 4.3 Which materials make a good filter – filter quality factor

As discussed above (Sect. 4.1), the selected sample materials showed not only a large variety of measured filtration efficiencies, but also of pressure drops. While some of the samples were already

hard to breathe through, others showed such small pressure drops that for a face mask several layers of this material could well be used to increase the overall filtration efficiency. The dependency of pressure drop and filtration efficiency on number of material layers (Sect. 4.2) allows a more comprehensive comparison of the capabilities of potential filter materials using the filter quality factor  $q_f$  (Hinds 1999; Huang et al. 2013):

$$q_f = \frac{\ln(\frac{1}{T})}{\Delta p}, \quad (6)$$

where  $T$  is the fractional transmission and  $\Delta p$  (in Pa) the pressure drop. Filter quality factors for the lower face velocity ( $v_f=5.3 \text{ cm s}^{-1}$ ) are summarized for small ( $d_p=30 \text{ nm} - 250 \text{ nm}$ ) and large ( $d_p=500 \text{ nm} - 10 \text{ }\mu\text{m}$ ) particles separately in Fig. 6a; those for the larger face velocity ( $v_f=12.9 \text{ cm s}^{-1}$ ) are shown in the SI in Fig. S23a.

Figure 6

Combining  $FE$  and  $\Delta p$  does not make the samples more similar: variability of filter quality factors is not smaller than that of  $FE$ . However, the order in which the various samples appear within the quality factor chart (reflecting the relative quality compared to other samples) has changed considerably compared to that of  $FE$  (Fig. 3). Especially several materials with very low pressure drop have moved towards the left end (“better” filtration characteristics) of the chart and replaced others with high  $FE$ , but also high  $\Delta p$ . As a consequence, in this chart also a number of regular household materials and fluffy textiles like French terry, fleece, microfiber cloth, felt, muslin or velour moved to the front end of the ranking, while several rather firm materials like poplin, surgical gown, or silk, but also one of the paper towel samples and the coffee filter moved towards the right end of the chart (i.e., “worse” filtration characteristics).

Filter quality factor is a rather abstract quantity. To present a more practical number which allows direct comparison of potential cloth mask materials, we use Eqs. 4 and 5 to calculate the hypothetical  $FE$  for each sample material for a cloth stack which would have the same pressure drop as surgical mask #1 as (arbitrarily selected) reference. In Fig. 6b we present these calculated filtration efficiencies for the smaller face velocity together with the hypothetical number of layers applied (Fig. S23b for the larger  $v_f$ ).

Filtration efficiencies for these hypothetical “reference pressure drop” masks reach high values for many sample materials, especially for the large particle size range. About two thirds of all masks would have filtration efficiencies  $>80\%$ . Depending on  $\Delta p$  at the individual layer, this would involve masks with often 4-7 layers and in some cases around 20 layers of material. Especially for materials with extremely low pressure drop at the single layer and very large thickness of the layer, this would result in very thick masks; e.g., the PU foam “reference pressure drop” mask would have 19 layers with a total thickness of more than 10 cm, which is quite impractical. Nevertheless, this comparison shows that using multiple layers of fabric would enable to produce cloth masks from many materials with reasonable filtration efficiency.

#### 4.4 Influence of material density on filtration efficiency

For individual pairs of materials we find larger filtration efficiency for the material with larger thread count than for the material with the smaller one, similar to the findings of Konda et al. (2020); however, this is not a general feature. When correlating  $FE$  with thread count (Fig. S25), we do not find a general relationship between these two variables, even when limiting the correlation to only a sub-group of materials (e.g., only cotton materials). This is probably because larger thread count is typically also related to thinner threads, which in turn reduces material thickness with negative

impact on  $FE$ . Also when correlating filter quality factor with thread count (Fig. S27), we do not find a strong dependency between these two variables, if at all a slight decrease in  $q_f$  with increasing thread count.

Filtration efficiency plotted versus material area density is presented in Fig. S24a and b for small and large particles, respectively. For small particles, no general trend was found for all samples. However, restricting the correlation to regular textiles, we find a general trend of increasing  $FE$  with increasing material area density. This increase is probably associated with increasing material thickness along these lines, associated with longer particle residence time within the filter material. For the large particles or for  $q_f$  (Fig. S26), however, we do not find such a relationship.

#### 4.5 Deposition by electrostatic attraction

Dedicated filtration materials as those used in respirators, surgical masks, or vacuum cleaner bags typically consist of non-woven fibers (Shimasaki et al. 2018) which carry permanent electrostatic charges to improve deposition of very small particles (Huang et al. 2013). To investigate the contribution of electrostatic attraction to overall particle removal, which likely caused enhanced  $FE$  for small, charged particles (Fig. 3a and Sect. 4.1), we use the measured filtration efficiency for the charged aerosol  $FE_{meas,charged}$  and of the neutralized aerosol  $FE_{meas,neutr}$ . With the fraction of charged particles  $X_{ch}(d_p)$  in charge equilibrium for the respective particle size  $d_p$  (Wiedensohler 1988) we calculate the filtration efficiency due to diffusion  $FE_{diff}$  and that due to electrostatic attraction ( $FE_{ES}$ ) according to:

$$FE_{diff} = \frac{FE_{meas,neutr} - X_{ch}(d_p) \cdot FE_{meas,charged}}{1 - X_{ch}(d_p)} \quad (7)$$

$$FE_{ES} = \frac{FE_{meas,charged} - FE_{diff}}{1 - FE_{diff}} \quad (8)$$

As a measure of the contribution of electrostatic attraction to overall  $FE$ , we calculate the ratio of  $FE_{ES}$  to  $FE_{diff}$  for each sample material, averaged for  $d_p=30$  nm – 100 nm, where we expect and observe enhanced  $FE$  for the charged aerosol. In Fig. 7 the electrostatic attraction-to-diffusion contribution ratio is presented for all samples, obtained at the lower face velocity ( $v_f=5.3$  cm s<sup>-1</sup>; measurements at the higher face velocity show a similar trend, however, are affected by stronger noise), sorted along decreasing  $FE_{ES}/FE_{diff}$  ratios.

Figure 7

For fourteen of the samples, mainly materials designed for filtration of particles like medical masks or vacuum cleaner bags, but also for triangle bandage, swimsuit material, French terry, flannel or velvet cotton, the contribution of electrostatic attraction to overall deposition is at least as large as the contribution by diffusion. Several other materials, mostly synthetic ones, also show significant electrostatic deposition, although at a lower level. Velvet cotton, silk and wool are some of the few non-synthetic materials for which we could identify substantial electrostatic contribution to overall deposition. Likely, electrostatic charge in these samples is not permanent but generated during handling of the material. For most samples consisting of natural fibers, we found only very small or negligible contributions to small-particle deposition by electrostatic attraction.

#### 4.6 How strongly do leaks affect filtration efficiency?

Surgical masks as well as cloth masks never have a perfect fit on the face. Leaks between the mask material and the skin allow air to pass through without being filtered by the mask material. This is one of the main reasons why in studies investigating filter efficiencies of masks under real life

conditions for surgical masks significantly lower filtration rates have been found compared to, e.g., N95 (similar to FFP2 or KN95) respirators (Grinshpun et al. 2009; Chu et al. 2020).

To obtain an estimate on the influence of leaks on overall filtration efficiency of the mask material we performed dedicated measurements with two sample materials with defined leaks. These materials, a surgical mask (surgical mask #4, not investigated in the previous sections) and the velvet cotton sample, were selected due to their relatively high filtration efficiency and good mechanical stability (to avoid unraveling of the leaks during the measurements) but with different pressure drops. Four samples were probed at  $v_f=5.3 \text{ cm s}^{-1}$ : a completely intact sample, and samples with 0.5%, 1%, and 2% of the sample area being punched out, in each case distributed over three holes across the sample. In addition, we measured  $FE$  of the “leaking” samples using a flow rate that generated the same pressure drop at the sample as the one observed for the measurement at  $v_f=5.3 \text{ cm s}^{-1}$  for the leak-free sample. Under these conditions, we assume that the face velocity through the filter material is the same in both cases and that the additional flow through the leaking sample passes through the holes.

Figure 8

Filtration efficiencies, normalized to those measured at the leak-free sample, plotted versus the relative leak area (Fig. 8) directly provide the relative reduction of the filtration efficiency due to the leaks. For particles with  $d_p \leq 2.5 \text{ }\mu\text{m}$  (solid lines in Fig. 8)  $FE$  decreases by 50% for a leak of 1% of the sample area and by about two thirds for a 2%-leak. The decrease is slightly higher for the velvet cotton sample (red traces), compared to the surgical mask sample (blue traces). This is because  $\Delta p$  at the velvet cotton sample is larger than at the surgical mask and consequently a larger fraction of the total flow passes through the holes instead of the sample material. For  $10 \text{ }\mu\text{m}$  particles (dashed lines in Fig. 8) the observed decrease in filtration efficiency is smaller compared to that for smaller particles. This suggests that the larger particles do not follow the flow streamlines into the holes as well as the smaller particles do, and more of them have to pass through the filter material. Estimates of the “separation efficiency” of the leaks (see Sect. S3 and Fig. S28 in the SI) suggest that this is the case for particles with  $d_p \geq 5 \text{ }\mu\text{m}$ , with increasing efficiency as particle size increases.

These measurements cannot be much more than a qualitative description of the effects of leaks on the overall filtration efficiency of face masks. The fractional flow through a leak and the leak separation efficiency depend not only on the relative leak area and pressure drop of the mask material, but also on other variables like shape and position of the leaks. Nevertheless, these measurements show that already very small leaks in the order of one percent of the total sample area can substantially reduce the overall filtration efficiency of a mask down to half or even less compared with the value of the material itself. Therefore, it is critical that the leak area is kept at a minimum. However, impaction of large particles on the mask surface will reduce the leak-related transmission of the largest droplets, e.g., from speaking, coughing or sneezing, at least to a certain degree. The relatively large droplet velocities of several meters per second (Chao et al. 2009) occurring in such processes will further support impaction losses within the leaking mask. To obtain more quantitative results on the influence of leaks, more dedicated and detailed experiments need to be performed.

## 5 Discussion

Several studies found in the literature focusing on efficacy or filtration performance of cloth face masks come to very different conclusions. Several authors observe that some of the cloth masks filter fine or ultrafine particles with similar or even better efficiency, compared to KN95 or N95 (both similar to FFP2) masks (Lustig et al. 2020; Konda et al. 2020). Contrary, others find that cloth masks provide only very low or at least significantly lower filtration efficiency compared to N95 or surgical masks (Shakya et al. 2017; Rengasamy et al. 2010; Bae et al. 2020; Davies et al. 2013).

Cloth mask filtration efficiencies larger than those found for N95 masks are not in agreement with our results, at least not for numbers of fabric layers as typically used in masks. We suspect that large filtration efficiencies for “virus-like nanoparticles” which were reported by Lustig et al. (2020) are mainly caused by the fact that these nanoparticles were applied to the filtration media suspended in droplets with typical sizes of 10 – 20  $\mu\text{m}$ . Therefore, filtration efficiency was not measured for nanoparticles but for relatively large droplets. Also results by Konda et al. (2020), who found better filtration efficiencies for combinations of cotton with silk, chiffon, and flannel than for a N95 mask over a large particle size range are hard to understand. According to filtration theory and to our measurements filtration efficiency for very small particles should increase as particle size decreases, whereas Konda et al. (2020) reported the opposite behavior for  $d_p < 80\text{ nm}$  for the N95 mask. Their results for several other cloth materials, however, are in good agreement with our findings, including the observation that multiple layers of cloth material result in significantly enhanced filtration efficiencies.

Rengasamy and coauthors (2010) found filtration efficiencies for various cloth masks and materials in the order of 10%-60% for polydisperse aerosols ( $d_p = 20\text{ nm} - 1000\text{ nm}$ ), which agrees well with our findings. Shakyia and coauthors (2017) observed filtration efficiencies between 40% and 80% with a filtration minimum around  $d_p = 500\text{ nm}$  for several cloth masks using monodisperse particles ( $d_p = 30\text{ nm} - 2.5\text{ }\mu\text{m}$ ), similar to our results. These authors, as well as Davies et al. (2013), found significantly larger filtration efficiency for surgical masks, compared to homemade masks, also in good agreement with our findings.

We found considerable differences in filtration efficiency for particles of different sizes but also between the individual samples. In addition, we observed large differences in pressure drop across the sample. For many materials, this allows stacking of several layers without reaching excessive pressure drop levels, with significantly improved filtration capability of the resulting cloth stack. Calculated filtration efficiencies for textile stacks with the same pressure drop as observed for a surgical mask reached very high values for large particles, i.e.,  $d_p \geq 500\text{ nm}$ , and still decent levels for the smaller particles for many sample materials, mainly for those which were designed to filter particles and for fluffy textiles like, e.g., French terry, fleece, felt, or velour.

Measurements with defined leaks in the samples revealed that leaks of only a few percent of the mask area will substantially degrade the overall mask filtration efficiency. Leaks next to the nose can be minimized using nose clips. However, leaks at the remaining circumference of the mask strongly depend on the shape of the mask. Cup-shaped or fold-up masks have the potential to fit better onto the face with less leak area than pleated masks like surgical masks, however for this purpose they need to have the right size.

The measurements of this study provide information on filtration efficiency and pressure drop at various face masks and potential mask materials under the conditions of the measurements. We did not apply a breathing cycle with up- and down-swelling flow rate. This would likely influence the absolute values of filtration efficiencies, however, we do not expect that this will strongly affect the intercomparison between different sample materials. We also did not humidify the air flow. Large relative humidity of the flow through the mask materials will likely cause a wetting of the material. This could alter the transmission of particles through the material, e.g., as a consequence of swelling of fibers when they get wet. We also did not investigate the effects of cleaning (e.g., washing) the sample materials on both, filtration efficiency and pressure drop. Neupane and coworkers (2019) have shown that filtration efficiency of cloth masks dropped by 20% after the fourth washing and drying cycle as a consequence of changed pore size and shape. Since homemade masks typically are washed and re-used many times, this effect as well as the influence of humidity should be more thoroughly studied in future experiments. Extreme flow situations, like coughing or sneezing which produce jets of particles moving at high velocities (Chao et al. 2009; Han et al. 2013; Liu and Novoselac 2014), have also not been studied here. We hypothesize that under such conditions, leaks

of the masks will open further, reducing the overall filtration efficiency – at least for the smaller particles which do not impact on the inner surface of the mask.

## 6 Summary

Filtration efficiencies ( $FE$ ) of face masks and potential mask materials were determined for particles ranging from  $d_p=30$  nm – 10  $\mu$ m. For this purpose, size-resolved particle number concentrations upstream and downstream the sample material were determined in two different setups while it was passed by the aerosol-laden air. In addition, the pressure drop ( $\Delta p$ ) across the samples was measured and the dependency of  $FE$  on face velocity, particle charge and number of sample layers was investigated.

A total of 48 different sample materials was tested. This included three regular surgical masks and an FFP2 respirator for comparison, several pure cotton and cotton mixed with synthetics textiles, synthetic cloths, but also a large variety of other materials which can be found in a regular household like PU foams, triangle bandage, paper towels or a coffee filter.

Generally, a large variety of filtration efficiencies was found and a filtration minimum was observed for particles between 50 nm and 500 nm diameter with typically larger filtration efficiency found for large particles ( $d_p > 2.5$   $\mu$ m), compared to small ones ( $d_p < 100$  nm). With increasing face velocity, we found a decrease in  $FE$  for small particles ( $d_p \leq 250$  nm) and an increase in  $FE$  for large particles ( $d_p \geq 2.5$   $\mu$ m) due to the different loss mechanisms involved.

Filtration efficiency and pressure drop measured for different numbers of material layers showed that each layer can be treated as individual filter. Total  $FE$  of the whole stack can readily be estimated by multiplying the individual transmission efficiencies ( $T=1-FE$ ), while total pressure drop ( $\Delta p$ ) is the sum of the individual pressure drops. This allows the use of the filter quality factor, which considers both,  $FE$  and  $\Delta p$  for comparison of stacked cloth materials. Calculations for hypothetical cloth stacks with similar pressure drop as observed for a surgical mask revealed that by stacking adequate numbers of layers of the various sample materials it is possible to obtain decent filtration efficiency using cloth materials.

From measurements of completely charged aerosols and aerosols in charge equilibrium we estimated the contribution of electrostatic attraction to overall deposition for the individual sample materials for small particles ( $d_p \leq 100$  nm). Fourteen of the sample materials, mainly synthetic materials but also one cotton and two cotton mixed with synthetic samples, showed an electrostatic deposition contribution which was at least as large as deposition by diffusion.

Measurements using samples with defined leaks covering 0.5% to 2% of the sample area showed substantial reduction in total filtration efficiency by 50% to two thirds of the value obtained with the leak-free sample. Particles of  $d_p \geq 5$   $\mu$ m tend not to follow the leak flow completely and are deposited on the samples to a certain degree.

Our measurements show that face masks made of cloth materials can reach decent filtration efficiency over a large particle size range, when stacked to an adequate number of layers, especially if materials designed to filter aerosol particles or fluffy textiles like, e.g., French terry, fleece, felt or velour were used. Total filtration efficiency and pressure drop can be estimated readily from the respective values for the individual layers, leaving labor-intensive measurements of textile combinations unnecessary. Besides these features, selection of cloths for home-made face masks must always consider that no harmful substances are released by the material, which was not part of this study. This might exclude some chemically treated household materials for this usage, like vacuum cleaner bags with antibacterial treatment. However, even the best filtration efficiency is

easily degraded if the mask does not have a good fit and a significant fraction of the respiratory air is permitted to pass through leaks between mask and face.

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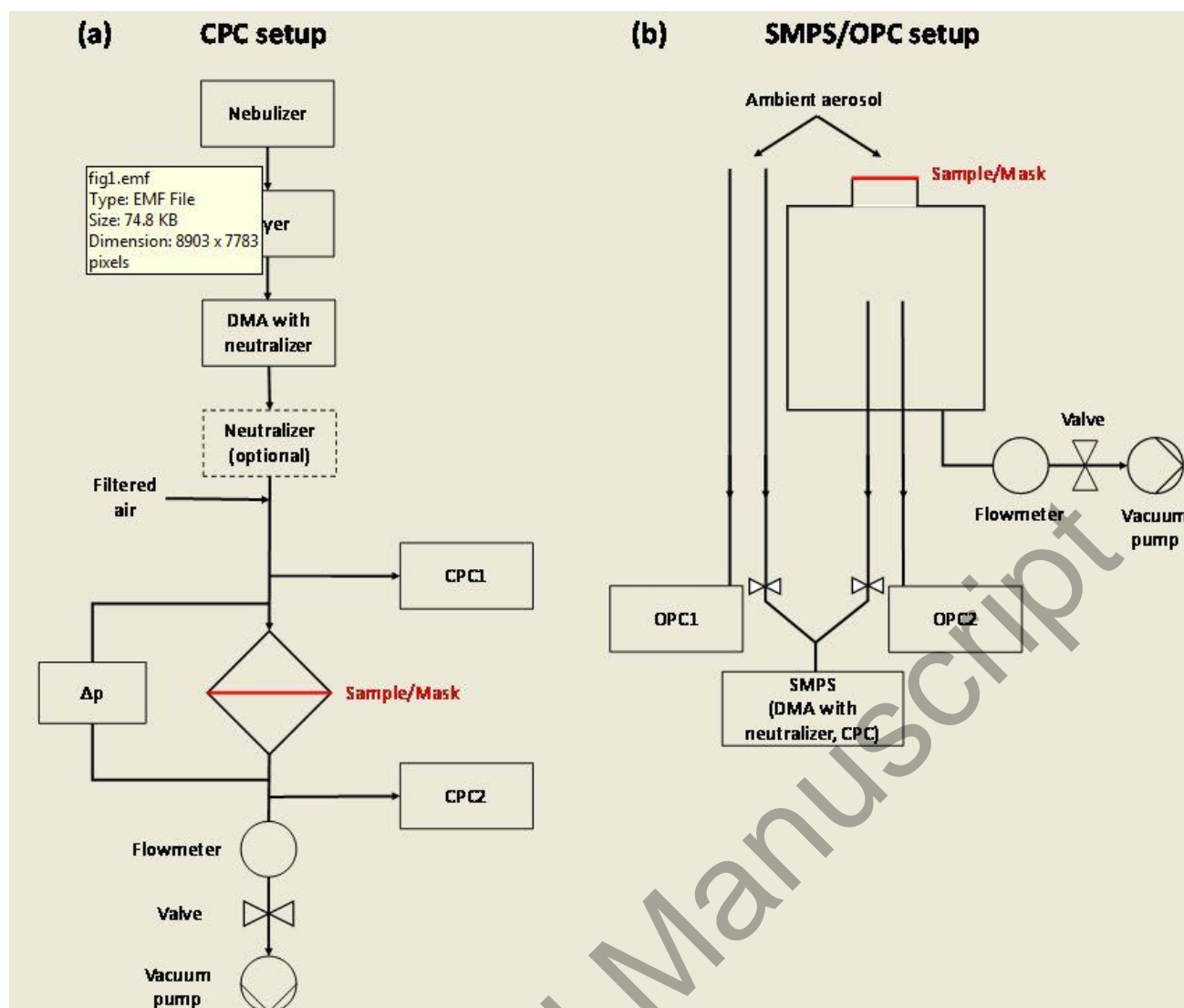


Figure 1: Experimental setups: a) *CPC setup*, b) *SMPS/OPC setup*.

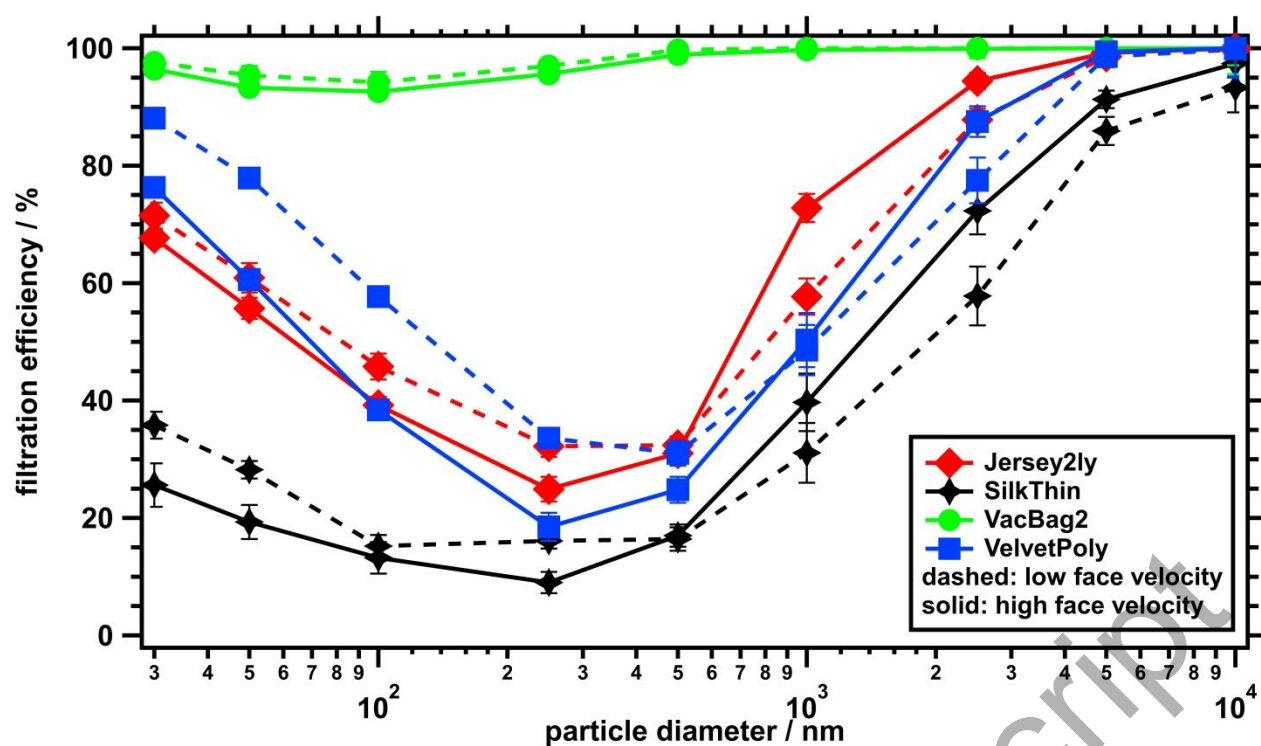


Figure 2: Filtration efficiency as a function of particle diameter measured using ambient aerosol (*SMPS/OPC setup*) at low ( $5.3 \text{ cm s}^{-1}$ , dashed lines) and high ( $12.9 \text{ cm s}^{-1}$ , solid lines) face velocity for cotton jersey (2 layers), thin silk, vacuum cleaner bag #2, and velvet polyester.

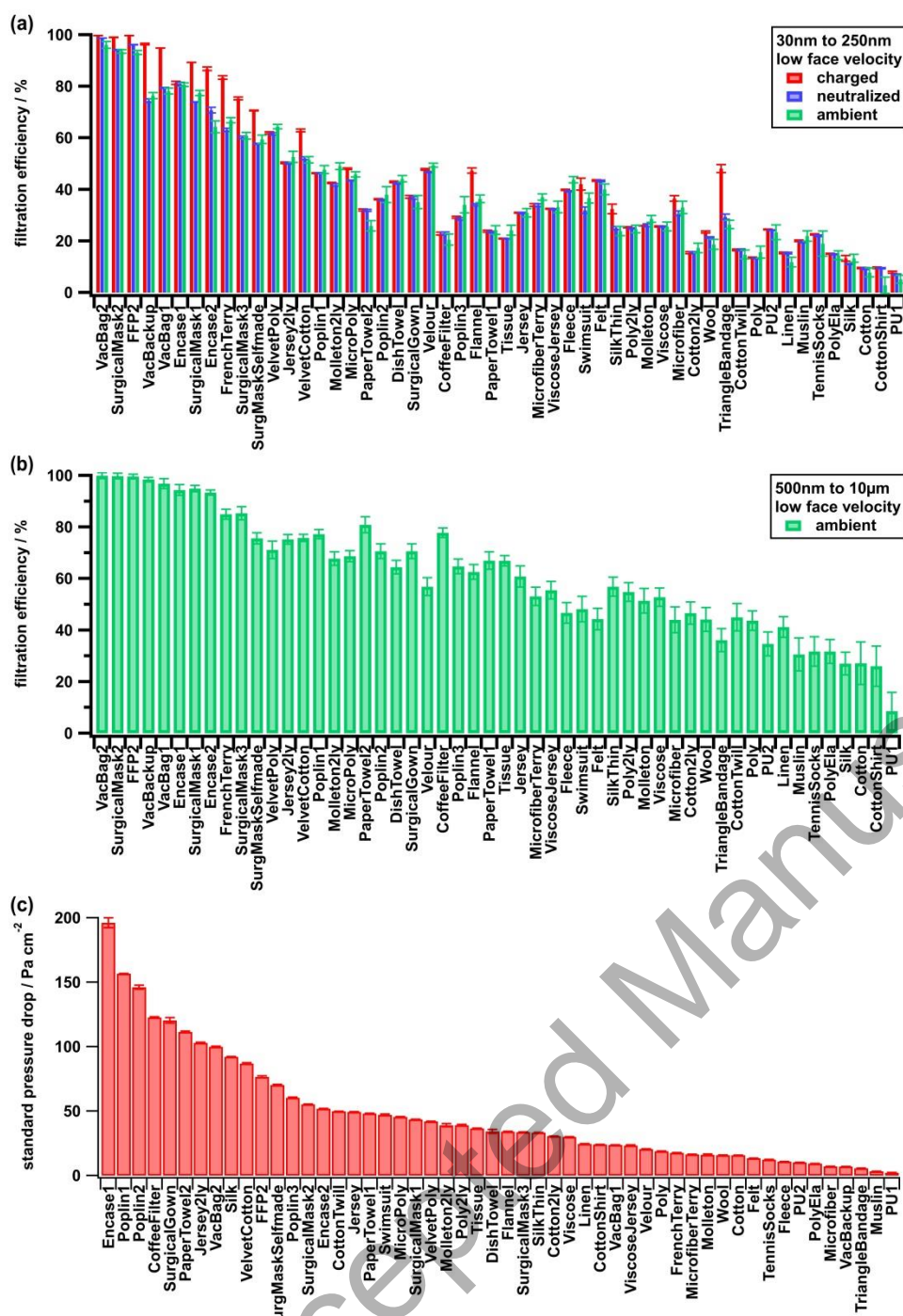


Figure 3: Filtration efficiencies measured at low face velocity ( $5.3 \text{ cm s}^{-1}$ ) for a) small particles ( $d_p=30$  to  $250 \text{ nm}$ ) in neutralized, charged (both *CPC setup*), and ambient (*SMPS/OPC setup*) aerosol, and for b) large particles ( $d_p=500 \text{ nm}$  to  $10 \mu\text{m}$ ) in ambient aerosol (*SMPS/OPC setup*). Values are sorted according to filtration efficiency averaged over all particle sizes. c) shows the standard pressure drop across the samples, sorted for decreasing values.

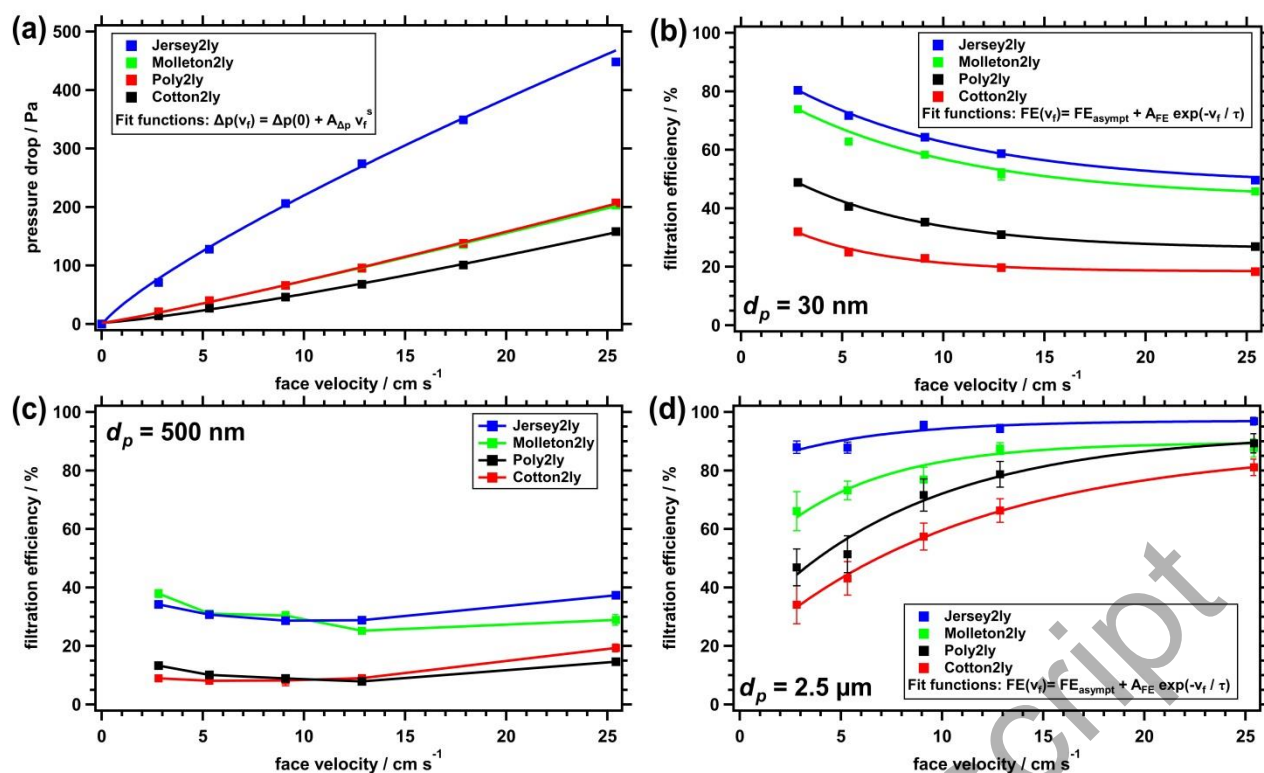


Figure 4: Dependence of a) pressure drop and b-d) filtration efficiencies at different particle sizes (30 nm, 500 nm, both neutralized aerosol, *CPC setup*; 2.5  $\mu\text{m}$ , ambient aerosol, *SMPS/OPC setup*) on face velocity for polyester, cotton woven, cotton jersey, and molleton (2 layers each). For the fitting coefficients, see Tables S2-S4.

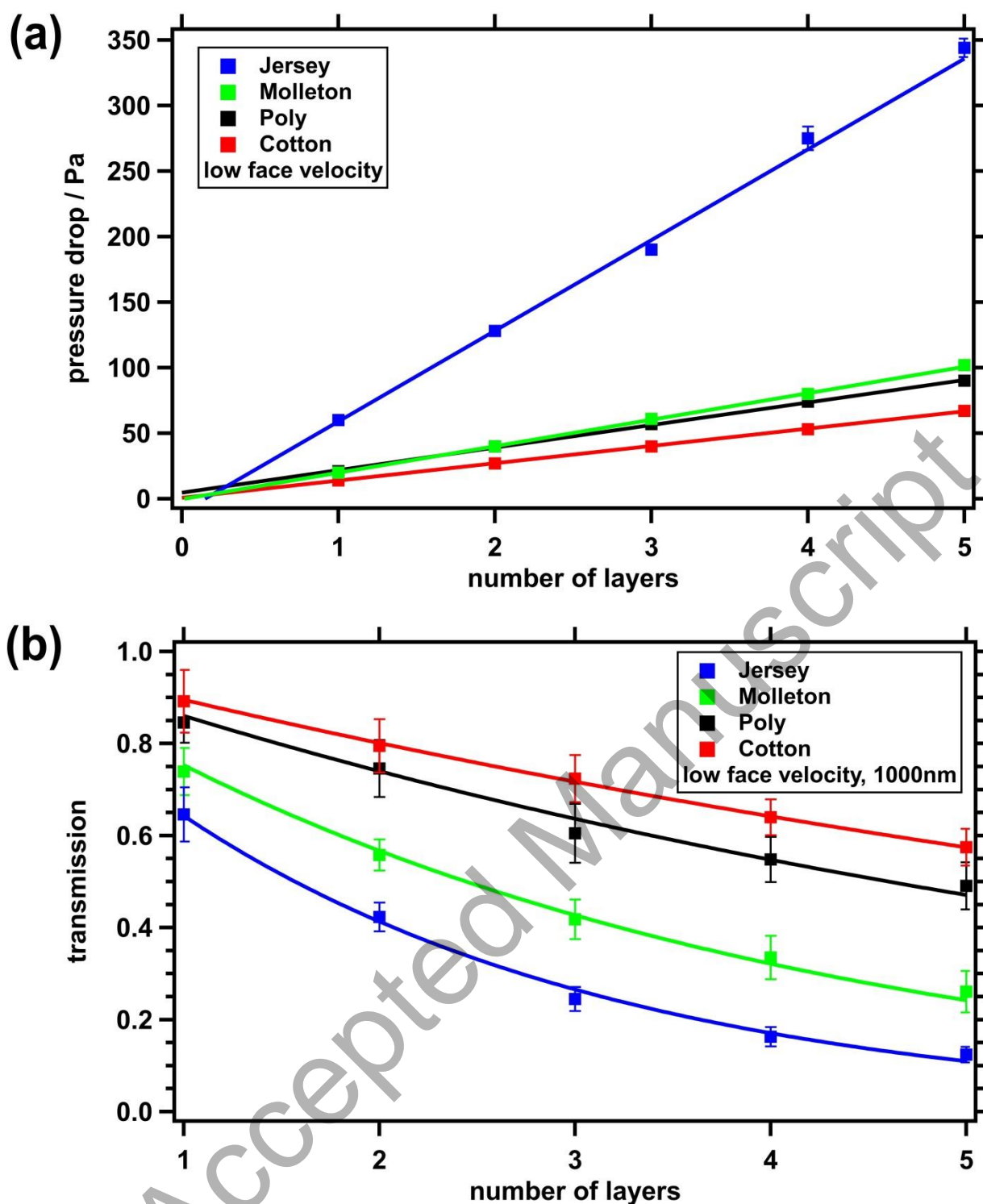


Figure 5: Dependence of a) pressure drop and b) transmission efficiency for 1  $\mu\text{m}$  particles on number of layers of the respective material (polyester, cotton woven, cotton jersey, and molleton), measured at low face velocity in ambient aerosol (*SMPS/OPC setup*). Fit coefficients can be found in Tables S5 (a) and S6 (b).



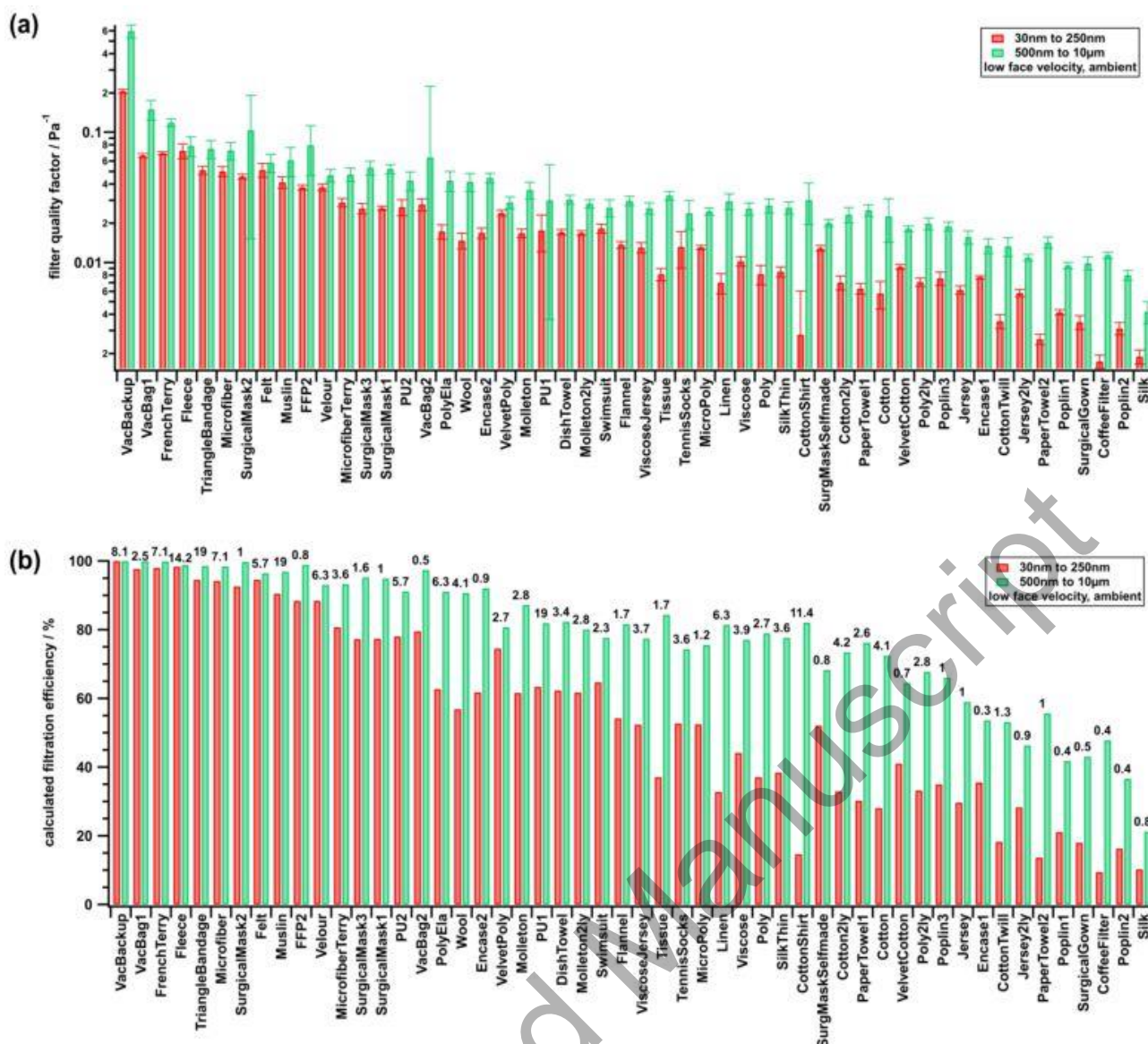


Figure 6: a) Filter quality factor  $q_f$  determined for small ( $d_p=30$  nm to 250 nm) and large ( $d_p=500$  nm to 10  $\mu$ m) particles in ambient aerosol (*SMPS/OPC setup*) at low face velocity. Values are sorted according to  $q_f$  averaged over all particle sizes. b) Calculated filtration efficiency for small and large particles (ambient aerosol, *SMPS/OPC setup*, low face velocity, sorted as in a)) for “reference pressure drop” cloth stacks. Above the bars the number of layers of this material is given which is needed to reach the reference pressure drop.



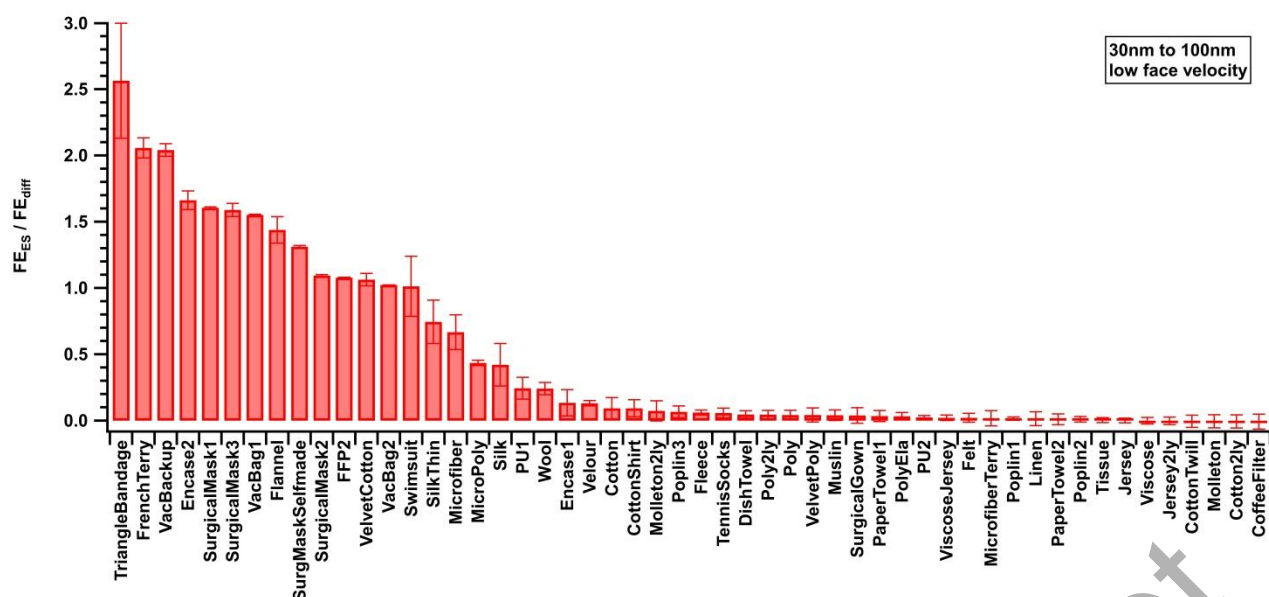


Figure 7: Ratio of filtration efficiencies due to electrostatic attraction ( $FE_{ES}$ ) to filtration efficiencies due to diffusion ( $FE_{diff}$ ) obtained at low face velocity for  $d_p \leq 100$  nm with the CPC setup, sorted for decreasing ratios.

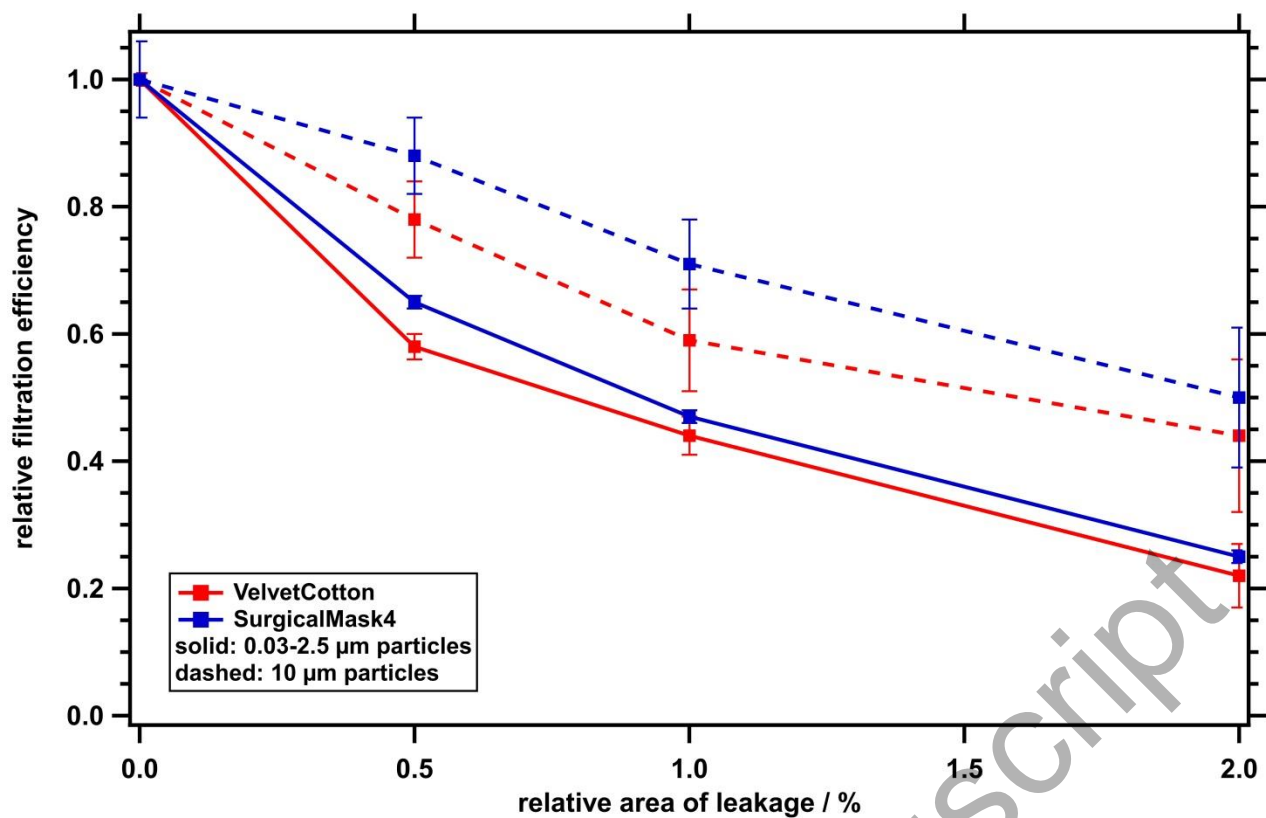


Figure 8: Filtration efficiency for velvet cotton (red) and surgical mask (blue) samples for  $d_p \leq 2.5 \mu\text{m}$  (solid line) and  $d_p = 10 \mu\text{m}$  (dotted line) versus relative leak area, normalized to the leak-free sample. Here, measurements of neutralized (*CPC setup*) and ambient aerosol (*SMPS/OPC setup*) were averaged, where available.